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(54) Title: LAYERED SMOOTH SURFACE ARAMID PAPERS OF HIGH STRENGTH AND PRINTABILITY			
(57) Abstract			
A multi-layered smooth surface aramid paper with high break strength and tear resistance comprises a substrate layer and at least one surface layer intimately bonded to the substrate layer, wherein the surface layer(s) consists essentially of 65 to 90 % by weight aramid fibrils and 10 to 35 % by weight aramid floc and comprises 10 to 67 % of the total basis weight of the paper.			

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TITLELAYERED SMOOTH SURFACE ARAMID PAPERS
OF HIGH STRENGTH AND PRINTABILITYBackground of the Invention

5 This invention relates to an improved layered aramid paper having a smooth surface and good tensile and tear strengths. The smooth surface provides for better print clarity and makes such papers particularly useful for high temperature label applications. Prior art
10 techniques that improve on surface smoothness often lead to a reduced level of mechanical strength and/or thermal stability. Moreover, synthetic papers which have been pressed or calendered at high temperature and pressure will generally have fibers on the surface which cause
15 roughness or snagging when the surface of the paper is worked during end use processing.

Summary of the Invention

20 This invention provides a multi-layered, smooth surface aramid paper containing from 40 to 55% by weight of fibrils and comprising a substrate layer which consists essentially of aramid fibrils and floc and one or two surface layers each intimately bonded to the substrate layer, said surface layer(s) consisting essentially of from 65 to 90% by weight aramid fibrils and from 10 to 35% by weight aramid floc and comprising from 10 to 67% of the weight of the paper. Preferably, the paper has a density of 0.8 to 1.0 g/cc with thickness of 1 to 30 mils (0.025 to 0.762 mm).
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Detailed Description of the Invention

The multi-layered aramid papers of the invention are comprised of layers of different compositions to provide desired properties. The surface layer(s) provide a smooth surface and contain from 65 to 90% aramid fibril and from 10% to 35% of aramid floc. The surface layer(s) constitutes from 10 to 67% of the weight of the paper. The substrate layer provides high tear strength. In order for

the multi-layered paper to behave as a unitary structure, it is preferred that the fibrous materials at the interface between layers be intermingled. This is achieved by depositing a layer of furnish, i.e., a paper-making aqueous dispersion of floc and fibrid on an undried, previously formed layer of furnish in a paper making machine or by simultaneously depositing the layers of different composition on the screen of the paper making machine using a 2 or 3 layer hydraulic type headbox. The paper coming off the machine is dried and calendered, preferably to a thickness of from 1 to 30 mils. The density of the layered paper is preferably from 0.8 to 1.0 g/cc for use as labels.

It has been found that the multi-layered papers of this invention have excellent mechanical properties. The smooth surface retains a high degree of smoothness even after the necessary working to prepare it for end use applications. This quality is important if print clarity and color density is to be achieved.

Aramid floc is high temperature resistant floc or short fiber cut from longer aramid fiber, such as those prepared by processes described in U.S. Pat. Nos. 3,063,966; 3,133,138; 3,767,756 and 3,869,430. It refers to short fibers typically having a length of 2 to 12 mm and a linear density of 1-10 decitex, made of aromatic polyamide which is non-fusible.

The aramid fibrids can be prepared using a fibridating apparatus where a polymer solution is precipitated and sheared in a single step as described in U.S. Pat. No. 3,756,908.

Tests and Measurements

Total Break Strength. The tensile break strength of paper is determined based on ASTM method D 828-87 for "Standard Test Method for Tensile Breaking Strength of Paper and Paperboard". Specimens are 2.54 cm wide and 20.3 cm long and the jaws of the tensile testing machine are initially separated by 12.7 cm. Ten paper samples are

tested in the machine direction (MD) and ten are tested in the cross direction (CD) and the values for each direction are averaged. The total of the MD and CD strengths is divided by paper density and paper basis weight to obtain 5 the Total Break Strength.

Thickness. Thickness of papers is determined using calipers in accordance with ASTM D 374-79 (1986).

Density. Density of papers is determined by determining the weight per unit area of the paper (Basis 10 Weight) in accordance with ASTM D 646-86 and dividing by the thickness.

Abraded Fiber Count.

In order to further investigate the abrasion qualities of these papers, the papers were folded and the 15 edge of the fold was viewed against a dark background. The number of fibers extending greater than about 0.5 mm above the solid paper surface was taken as the Abraded Fiber Count (per centimeter) and indicates the degree of roughness of the sample.

20 The following examples are illustrative of the invention and are not to be construed as limiting.

EXAMPLES

Example 1

25 A two layered structure was made by combining fibrils of poly(m-phenylene isophthalamide) prepared as described in Example 1 of U.S. Pat. No. 3,756,908 and floc prepared by dry spinning poly(m-phenylene isophthalamide) from a solution containing 67% dimethyl acetamide (DMAc), 30 9% calcium chloride and 4% water. The spun filaments were flooded with an aqueous liquid and contained about 100% DMAc, 45% calcium chloride and 30-100% water based on dry polymer. The filaments were washed and drawn 4X in an extraction-draw process in which the chloride and DMAc 35 contents were reduced to about 0.10% and 0.5%, respectively. The filaments had a denier of 2 (2.2 dtex) and typical properties were: elongation to break, 34%, and tenacity, 4.3 grams/denier (3.8 dN/tex). The filaments

were then cut to floc length of 0.27 inch (0.68 cm) and slurried in water to a concentration of about 0.35%.

Blends of fibrils and floc were separately fed to a 2-layer hydraulic type headbox which maintains each 5 blend as a distinct layer until the slice exit where limited mixing of the layers occurs. This allows good bonding between the layers while still maintaining the individual nature of each layer. The formed sheet is then processed as is normally done on a fourdrinier paper 10 machine by pressing and drying.

The papers are dried completely using infrared heaters before being calendered at 320°C at a line speed of 30 feet per minute (9 meters per minute) using a pressure of 725 pounds per linear inch (130 kg/cm).

15 The composition of the layers varied from 35 to 65% fibril, the remainder being floc. The basis weight of each layer was adjusted so that the high fibril layer (65% fibril) ranged from 33 to 67% of the total basis weight of the final sheet. The total fibril content of the test 20 papers ranged from 45 to 55% of the sheet versus 53% for the single layer control papers (C1-1). Table 1 gives the basis weight of each layer and its composition.

Table 1

Run Number	Total Sheet			Substrate Layer			Surface Layer			
	BW aim g/m ²	% Fibril	% Floc	BW aim g/m ²	% Fibril	% Floc	BW aim g/m ²	% Fibril	% Floc	
30	1-1	42	45	55	28	35	65	14	65	35
	1-2	42	50	50	21	35	65	21	65	35
	1-3	42	55	45	14	35	65	28	65	35
35	C1-1	42	53	47	42	53	47	-	-	-

40 The amount of loose fibers on the surfaces of the sheet as a result of mechanical working of the calendered paper was measured (Table 2). Side 1 is the substrate layer (low fibril content layer) and Side 2 the surface (high fibril content) layer.

Table 2
Abraded Fiber Count

	Sample Number	Fiber Count (per 5 cm)	
		Side 1	Side 2
5	1-1	20	0
10	1-2	12	2
	1-3	14	0
15	C1-1	14	-

Even with the significant reduction in the number of loose fibers on the surface of the high fibrill content papers, superior mechanical properties are maintained versus a control paper of similar average composition but with no layering (Table 3).

Table 3
Calendered Paper Properties

	Sample Number	1-1	1-2	1-3	C1-1
25	B.W.*, oz/yd ² (g/m ²)	1.3 (44.1)	1.5 (50.9)	1.4 (47.5)	1.3 (44.1)
	Thickness, mils (mm)	2.0 (0.051)	2.5 (0.064)	2.2 (0.056)	2.4 (0.061)
30	Density, g/cc	0.82	0.89	0.86	0.72
	B.S.**, 1b/in MD/CD (N/cm)	15/7 (26/12)	21/10 (37/18)	18/7 (32/12)	20/8 (35/14)
	Eb***, MD/CD	4/3	6/3	5/2	6/3
35	Elmendorf Tear, g MD/CD (N)	108/191 (1.06/1.87)	120/193 (1.18/1.89)	87/166 (0.85/1.63)	127/215 (1.25/2.11)
	Shrinkage @ 300°C, % MD/CD	2/0	2/0	2/0	2/0

40 * Basis Weight

** Break Strength

*** Break Elongation

Example 2

Layered structures, 4.0-4.5 oz/yd² (135.6-152.6 g/m²) were produced with high fibrid layers on both top and bottom of the structure. The top and bottom plies (outer layers) had equal basis weight. The top and bottom layers contain 65% fibrid and 35% floc. The top layer was applied using a secondary headbox jetting the furnish onto an already formed sheet which was prepared using the headbox of Example 1. The control (C2-1) was a single layer paper.

Table 4

Run Number	Total Sheet			Each Outer Layer			Inner (Substrate) Layer		
	BW aim g/m ²	% Fibrid	% Floc	BW aim g/m ²	% Fibrid	% Floc	BW aim g/m ²	% Fibrid	% Floc
2-1	132	46	54	24	65	35	84	35	65
2-2	132	55	45	44	65	35	44	35	65
C2-1	137	47	137	53	47	-	-	-	-

Improvement in the amount of loose fibers on the surface as a result of mechanical working of the paper is obvious from Table 5.

Table 5

Abraded Fiber Count

	Sample Number	Fiber Count (per 5 cm)
	2-1	5
	2-2	7
	C2-1	12

Even with the major reduction in the number of loose fibers on the surface of the papers superior mechanical properties are maintained versus a control paper of similar average composition but with no layering

(Table 6). The low shrinkage at 300°C along with the high tear and tensile properties as compared with the control is especially noteworthy.

5

Table 6
Calendered Paper Properties

	<u>Sample Number</u>	<u>2-1</u>	<u>2-2</u>	<u>C2-1</u>
	Basis Weight, oz/yd²	4.3	4.3	4.1
10	(g/m ²)	(145.7)	(145.8)	(139.0)
	Thickness, mils	7.5	6.7	6.8
	(mm)	(0.191)	(0.170)	(0.173)
	Density, g/cc	0.77	0.87	0.80
15	B.S., lb/in MD/CD	55/30	61/39	54/33
	(N/cm)	(96/53)	(107/68)	(95/58)
	Eb, % MD/CD	6/4	9/6	7/5
	Elmendorf Tear, g MD/CD	695/762	421/598	504/662
	(N)	(6.82/7.48)	(4.13/5.87)	(4.94/6.49)
20	Shrinkage @300°C, % MD/CD	1/1	1/1	1/1

Claims:

1. A multi-layered smooth surface aramid paper containing from 40 to 55% by weight of fibrils and comprising a substrate layer which consists essentially of 5 aramid fibrils and floc and one or two surface layers, each intimately bonded to the substrate layer, said surface layer(s) comprising from 10 to 67% of the weight of the paper and consisting essentially of from 65 to 90% by weight aramid fibrils and from 10 to 35% by weight 10 aramid floc;
2. The paper of Claim 1 having a density of 0.8 to 1.0 g/cc and a thickness of 1 to 30 mils (0.0254 to 0.762 mm).
15
3. The paper of Claim 1, wherein said paper comprises two surface layers intimately bonded to opposite sides of said substrate layer.

INTERNATIONAL SEARCH REPORT

International Application No.
PCT/US 94/14672A. CLASSIFICATION OF SUBJECT MATTER
IPC 6 D21H13/26

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 6 D21H

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
P, X	WO,A,94 16142 (DU PONT DE NEMOURS) 21 July 1994 *The entire abstract* ---	1-3
X	US,A,5 089 088 (G.L.HENDREN ET AL) 18 February 1992 see claims 1-6 ---	1-3
A	US,A,5 076 887 (G.L.HENDREN) 31 December 1991 see claims 1-17 ---	1-3

 Further documents are listed in the continuation of box C. Patent family members are listed in annex.

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Patent document cited in search report	Publication date	Patent family member(s)		Publication date
WO-A-9416142	21-07-94	NONE		
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